

Mine Drop Experiment (MIDEX)



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Republic of Korea minesweeper *YMS-516* is blown up by a magnetic mine, during sweeping operations west of Kalma Pando, Wonsan harbor, on 18 October 1950.

From http://www.history.navy.mil/photos/events/kowar/50-unof/wonsan.htm

Acknowledgements

- Chenwu Fan
- Marla Stone
- ET1 Adam Dummer
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- Prof. Chu

Overview

- Mine Warfare Overview
- Important Environmental Parameters for MCM Operations
- Impact Burial Prediction Model
- Mine Drop Experiment Overview
- Hydrodynamic Theory
- Data Analysis
- Conclusion
- Questions

A Shift in Operational Focus

- Breakdown of Soviet Union Forced Change in U.S. Navy Mission Requirements.
- Primary Guiding Documents: ... From the Sea, Forward ... From the Sea, Operational Maneuver from the Sea.
- Shift in Mission Focus from Open Ocean to the Littoral.
- Greatest Threat to U.S. Forces Operating in the Littoral: the Naval Mine.

Naval Mine Characteristics

Characterized by:

- Method of Delivery: Air, Surface or Subsurface.
- Position in Water Column: Bottom, Moored or Floating.
- *Method of Actuation*: Magnetic and/or Acoustic Influence, Pressure, Controlled or Contact.

- Composed of metal or reinforced fiberglass.
- Shapes are Typically Cylindrical but Truncated Cone (Manta) and Wedge (Rockan) shaped mines exist.

Naval Mine Threat

Inexpensive Force Multiplier

Roberts (FFG-58), Tripoli (LPH-10), Princeton (CG-59)

Damages \$125 Million; Mines Cost \$30K

Numerous Types

Widely Available

- •Over 50 Countries (40% Increase in 10 Yrs)
 - Over 300 Types (75% Increase in 10 Yrs)
 - 32 Countries Produce (60% Increase in 10 Yrs)
 - 24 Countries Export (60% Increase in 10 Yrs)

WWII Vintage to Advanced Technologies (Multiple Sensors, Ship Count Routines, Anechoic Coatings Non-Ferrous Materials)

Important Environmental Parameters for MCM Operations

- Water Properties
- Weather
- Beach Characteristics
- Tides and Currents
- Biologics
- Magnetic Conditions
- Bathymetry (Bottom Type)

Impact Burial

- Mine Impacting Bottom will Experience a Certain Degree of "Impact Burial (IB)".
 - Highest Degree of IB in Marine Clay and Mud.
 - IB Depends on Sediment Properties, Object's Impact Orientation, Shape and Velocity.
- MCM Doctrine Provides only a Rough Estimate of IB.

Bottom	Predicted Mine Bottom		Bottom
Composition	Case Burial %	Roughness	Category
		Smooth	В
Rock	0	Moderate	С
		Rough	С
MUD OR SAND		Smooth	Α
	0 TO 10	Moderate	В
		Rough	С
		Smooth	Α
	10 TO 20	Moderate	В
		Rough	С
		Smooth	Α
	25 TO 75	Moderate	В
		Rough	С
	75 TO 100	All	С

Development of Navy's Impact Burial Prediction Model (IBPM)

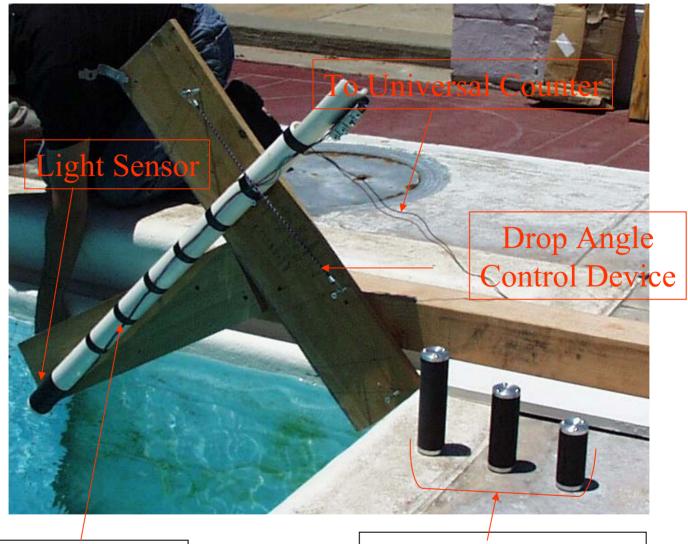
- IBPM was designed to calculate mine trajectories for air, water and sediment phases.
- Arnone & Bowen Model (1980) Without Rotation.
- Improved IBPM (Satkowiak, 1987-88) With Rotation.
- Final Improvements made by Hurst (1992):
 - More Accurately Calculates Fluid Drag and Air-Sea and Sea-Sediment Interface Forces.
 - Treats Sediment as Multi-Layered.

Impact 25

- Main Limitations:
 - 1. Model assumes mine body is of uniform density, thus center of buoyancy coincides with center of mass.
 - 2. Model numerically integrates momentum balance equations only. Does not consider moment balance equations.
- If a mine's water phase trajectory is not accurately modeled, then IB predictions will be wrong.
- Recent sensitivity studies by (Chu et al., 1999, 2000, Taber 1999, Smith 2000) have only focused on sediment phase calculations.

MIDEX

- MIDEX designed to examine the uniform density assumption of IMPACT 25, namely what effect a varying center of mass will have on a mine shape's water phase trajectory.
- Controlled Parameters:
 - 1. Drop Angles: 15°, 30°, 45°, 60°, 75°.
 - 2. Center of Mass Position.
 - 3. L/D ratio (constant).
 - 4. V_{init} (to some extent).
- Conducted several tests for each drop angle, center of mass position and initial velocity.

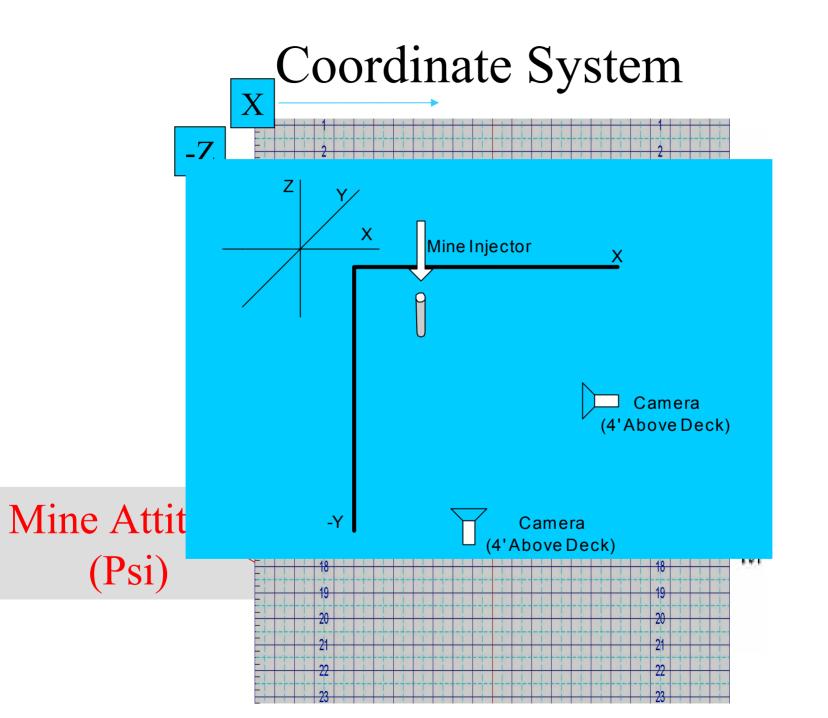


Mine Injector

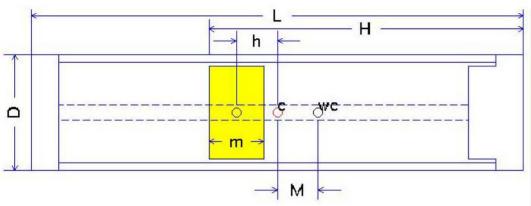
Mine Shapes:

Length: 15, 12, 9 cm

Diameter: 4 cm



Center of Mass





L=15.1359cm D=4cm m=2.7cm Weight=322.5 g Volume=190.2028 cm³ Density=1.6956 g/cm³

> H: 10.380 8.052 5.725 cm h: -1.462 0.866 3.193 cm M: 0.000 18.468 36.935 mm

> > MODEL # 2

L=12.0726cm D=4cm m=1.7cm

Weight=254.2 g Volume=151.709 cm3 Density=1.6756 g/cm3

H: 8.450 6.609 4.768 cm h: -1.564 0.277 2.119 cm M: 0.000 12.145 24.290 mm

MODEL#3

L=9.1199cm D=4cm m=1.47cm

Weight=215.3 g Volume=114.6037 cm3 Density=1.8786 g/cm3

H: 6.662 5.592 4.521 cm h: -1.368 -0.297 0.774 cm M: 0.000 6.847 13.694 mm



Defined COM position as:

2 or -2: Farthest from volumetric center 1 or -1

0: Coincides with volumetric center

 Solid Body Falling Through Fluid Should Obey 2 Physical Principles:

$$\int (dV^* / dt^*) dm^* = W^* + F_b^* + F_d^*$$

2. Moment of Momentum Balance

$$\int [r^* \times (dV^* / dt^*)] dm^* = M^*$$

* Denotes dimensional variables

 $V^* \rightarrow Velocity$

 $W^* \rightarrow gravity$

 $F_b^* \rightarrow buoyancy force$

 $F_d^* \rightarrow drag force$

 $M^* \rightarrow resultant moment$

 Considering both momentum and moment of momentum balance yields 9 governing equations that describe the mine's water phase trajectory.

$$\frac{dV_{1}}{dt} + \omega_{2}V_{3} - \omega_{3}V_{2} = -\frac{C_{D}\rho_{w}}{2\rho_{m}} | \overrightarrow{V}| (V_{1} - V_{w1}) + \frac{\rho_{m} - \rho_{w}}{\rho_{m}} \cos \psi_{1}$$

$$\left| \frac{dV_1}{dt} + \omega_2 V_3 - \omega_3 V_2 \right| = -\frac{C_D \rho_w}{2\rho_m} |\vec{V}| (V_1 - V_{w1}) + \frac{\rho_m - \rho_w}{\rho_m} \cos \psi_1 \left| \frac{dV_2}{dt} + \omega_3 V_1 - \omega_1 V_3 \right| = -\frac{C_D \rho_w}{2\rho_m} |\vec{V}| (V_2 - V_{w2}) + \frac{\rho_m - \rho_w}{\rho_m} \cos \psi_2 \left| \frac{dV_2}{dt} + \omega_3 V_1 - \omega_1 V_3 \right| = -\frac{C_D \rho_w}{2\rho_m} |\vec{V}| (V_2 - V_{w2}) + \frac{\rho_m - \rho_w}{\rho_m} \cos \psi_2 \left| \frac{dV_2}{dt} + \omega_3 V_1 - \omega_1 V_3 \right| = -\frac{C_D \rho_w}{2\rho_m} |\vec{V}| (V_2 - V_{w2}) + \frac{\rho_m - \rho_w}{\rho_m} \cos \psi_2 \left| \frac{dV_2}{dt} + \omega_3 V_1 - \omega_1 V_3 \right| = -\frac{C_D \rho_w}{2\rho_m} |\vec{V}| (V_2 - V_{w2}) + \frac{\rho_m - \rho_w}{\rho_m} \cos \psi_2 \left| \frac{dV_2}{dt} + \omega_3 V_1 - \omega_1 V_3 \right| = -\frac{C_D \rho_w}{2\rho_m} |\vec{V}| (V_2 - V_{w2}) + \frac{\rho_m - \rho_w}{\rho_m} \cos \psi_2 \left| \frac{dV_2}{dt} + \omega_3 V_1 - \omega_1 V_3 \right| = -\frac{C_D \rho_w}{2\rho_m} |\vec{V}| (V_2 - V_{w2}) + \frac{\rho_m - \rho_w}{\rho_m} \cos \psi_2 \left| \frac{dV_2}{dt} + \omega_3 V_1 - \omega_1 V_3 \right| = -\frac{C_D \rho_w}{2\rho_m} |\vec{V}| (V_2 - V_{w2}) + \frac{\rho_m - \rho_w}{\rho_m} \cos \psi_2 \left| \frac{dV_2}{dt} + \omega_3 V_1 - \omega_1 V_3 \right| = -\frac{C_D \rho_w}{2\rho_m} |\vec{V}| (V_2 - V_{w2}) + \frac{\rho_m - \rho_w}{\rho_m} \cos \psi_2 \left| \frac{dV_2}{dt} + \omega_3 V_1 - \omega_1 V_3 \right| = -\frac{C_D \rho_w}{2\rho_m} |\vec{V}| (V_2 - V_{w2}) + \frac{\rho_m - \rho_w}{\rho_m} \cos \psi_2 \left| \frac{dV_2}{dt} + \omega_1 V_1 - \frac{Q_1 V_2}{2\rho_m} |\vec{V}| (V_2 - V_{w2}) + \frac{\rho_m - \rho_w}{\rho_m} \cos \psi_2 \left| \frac{dV_2}{dt} + \frac{Q_1 V_2}{2\rho_m} |\vec{V}| (V_2 - V_{w2}) + \frac{\rho_m - \rho_w}{\rho_m} \cos \psi_2 \left| \frac{dV_2}{dt} + \frac{Q_1 V_2}{2\rho_m} |\vec{V}| (V_2 - V_{w2}) + \frac{Q_1 V_2}{\rho_m} |\vec{V}| (V_2 - V_$$

$$\left| \frac{dV_3}{dt} + \omega_1 V_2 - \omega_2 V_1 = -\frac{C_D \rho_w}{2\rho_m} | \vec{V} | (V_3 - V_{w3}) + \frac{\rho_m - \rho_w}{\rho_m} \cos \psi_3 \right|$$

$$J_1 \frac{d\omega_1}{dt} + (J_3 - J_2)\omega_2\omega_3 - J_{31}(\frac{d\omega_3}{dt} + \omega_1\omega_2) = \frac{LM_1^*}{g}$$

$$J_2 \frac{d\omega_2}{dt} + (J_1 - J_3)\omega_3\omega_1 - J_{31}(\omega_3^2 - \omega_1^2) = \frac{LM_2^*}{g}$$

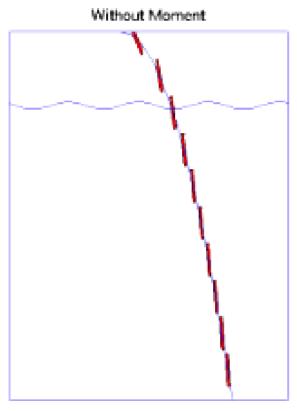
$$J_2 \frac{d\omega_2}{dt} + (J_1 - J_3)\omega_3\omega_1 - J_{31}(\omega_3^2 - \omega_1^2) = \frac{LM_2^*}{g}$$

$$J_{3} \frac{d\omega_{3}}{dt} + (J_{2} - J_{1})\omega_{1}\omega_{2} - J_{31}(\frac{d\omega_{1}}{dt} - \omega_{2}\omega_{3}) = \frac{LM_{3}^{*}}{g}$$

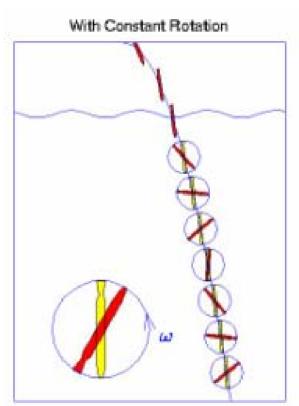
$$\left| \frac{d}{dt} \cos \psi_1 = \omega_3 \cos \psi_2 - \omega_2 \cos \psi_3 \right| \qquad \left| \frac{d}{dt} \cos \psi_2 = \omega_1 \cos \psi_3 - \omega_3 \cos \psi_1 \right| \qquad \left| \frac{d}{dt} \cos \psi_3 = \omega_2 \cos \psi_1 - \omega_1 \cos \psi_2 \right|$$

$$\frac{d}{dt}\cos\psi_2 = \omega_1\cos\psi_3 - \omega_3\cos\psi_1$$

$$\frac{d}{dt}\cos\psi_3 = \omega_2\cos\psi_1 - \omega_1\cos\psi_2$$

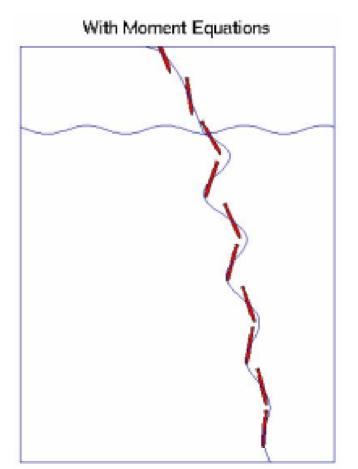


Arnone-Bowen IBPM Without Moment Equation



Improved IBPM with rotation but without Moment Equation

• By considering both equations mine will exhibit a spiral fall pattern.



Data Analysis

- 1. Video converted to digital format.
- 2. Digital video from each camera analyzed frame by frame (30Hz) using video editing program.
- 3. Mine's top and bottom position determined using background x-z and y-z grids. Positions manually entered into MATLAB for storage and later processing.
- 4. Analyzed 2-D data to obtain mine's x,y and z center positions, attitude (angle with respect to z axis) and u,v, and w components.

Non-dimensional Conversions

• In order to generalize results, data was converted to non-dimensional numbers.

$$t^* = \frac{dt}{\sqrt{\frac{L}{g}}}, V_i^* = \frac{V_i}{\sqrt{gL}}, \frac{L}{D}, COM = \frac{2\Delta L}{L}, \frac{(x,y,z)}{L}, \frac{(u,v,w)}{\sqrt{gL}}$$

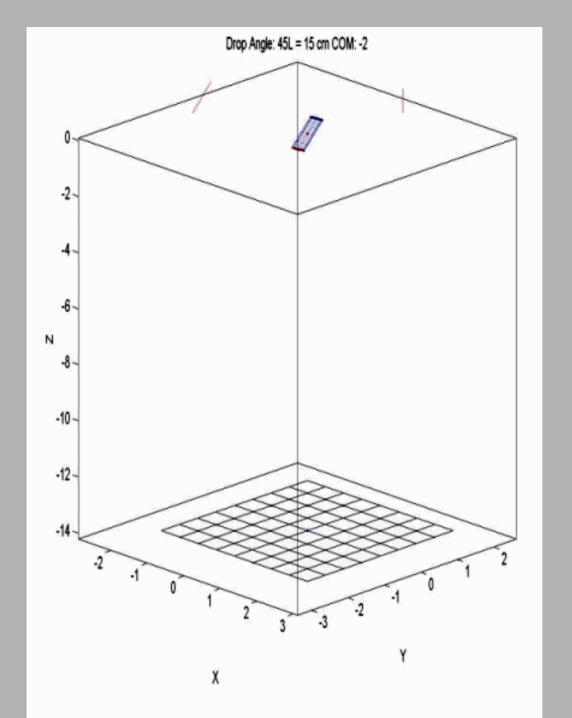
Sources of Error

- 1. Grid plane behind mine trajectory plane. Results in mine appearing larger than normal.
- 2. Position data affected by parallax distortion and binocular disparity.
- 3. Air cavity affects on mine motion not considered in calculations.
- 4. Camera plane not parallel to x-y plane due to pool slope.

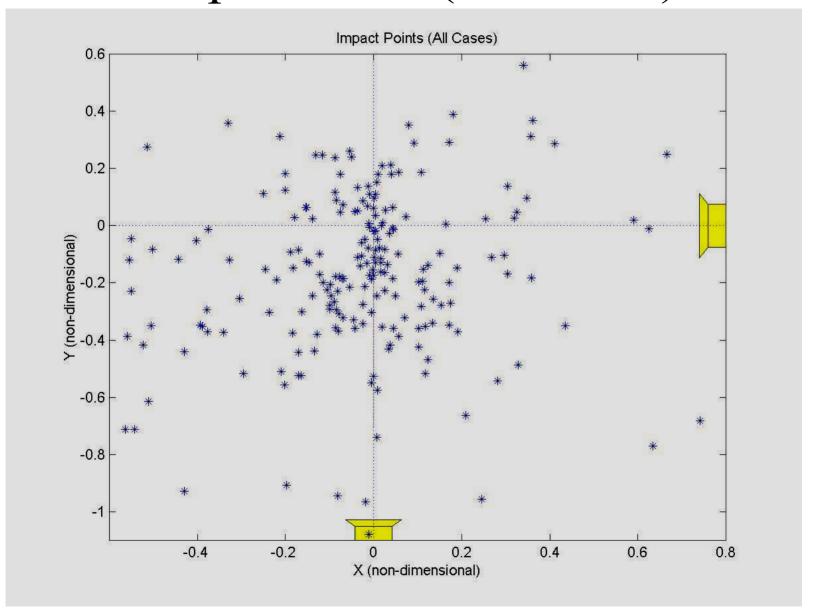
Underwater Video Clip

Center of Mass: Position 2

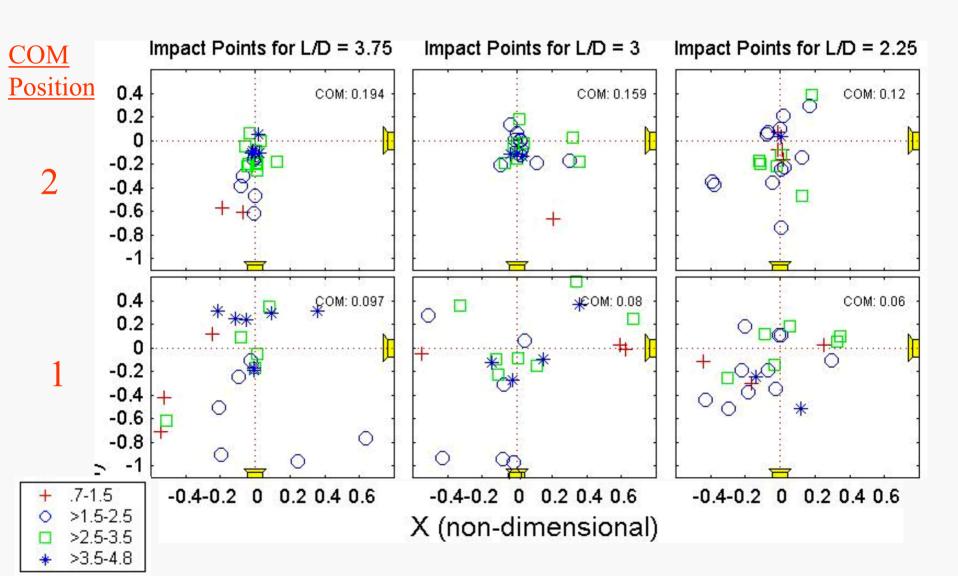
Drop Angle: 45; L= 15cm; Vi= 2.874m/s; COM: -2 Drop Angle: 45; L= 15cm; Vi= 2.874m/s; COM: -2 0 0 -0.2 -0.4 -0.5 -0.6 -0.8 -1 Z (m) Z (m) -1.2 -1.4 -1.5 -1.6 -1.8 -2 -2 -0.4 -0.2 0 0.2 -0.8 -0.6 0.2 -0.2 0 0.4 0.6 Y (m) X (m)

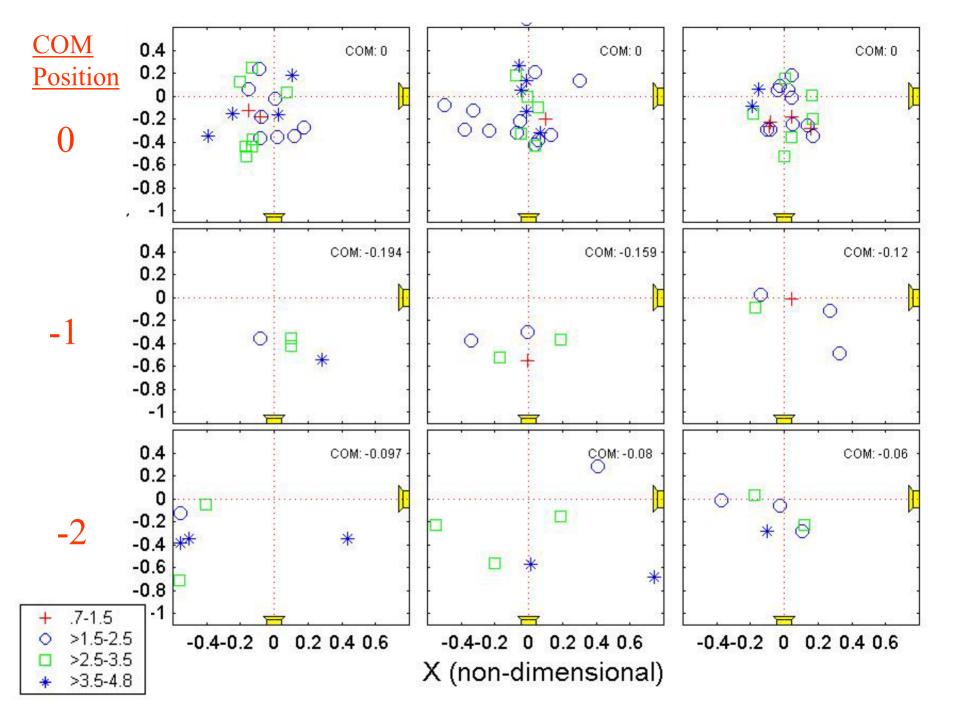


Impact Point (All Cases)

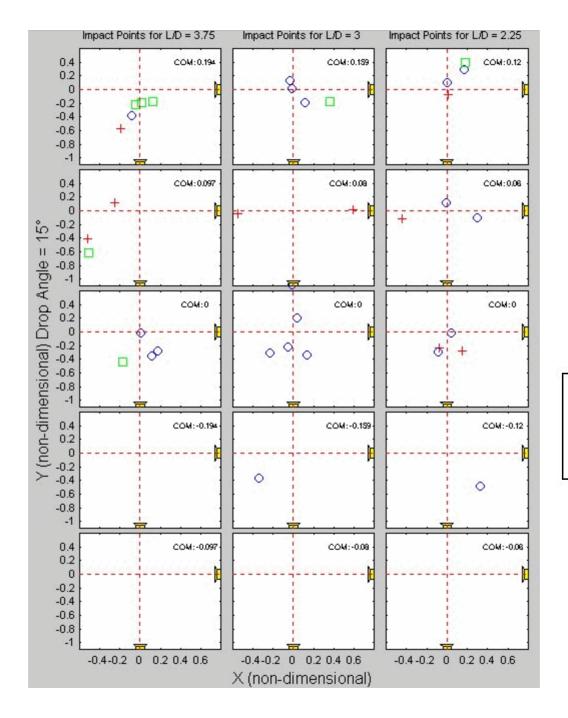


Impact Point (All Drop Angles)



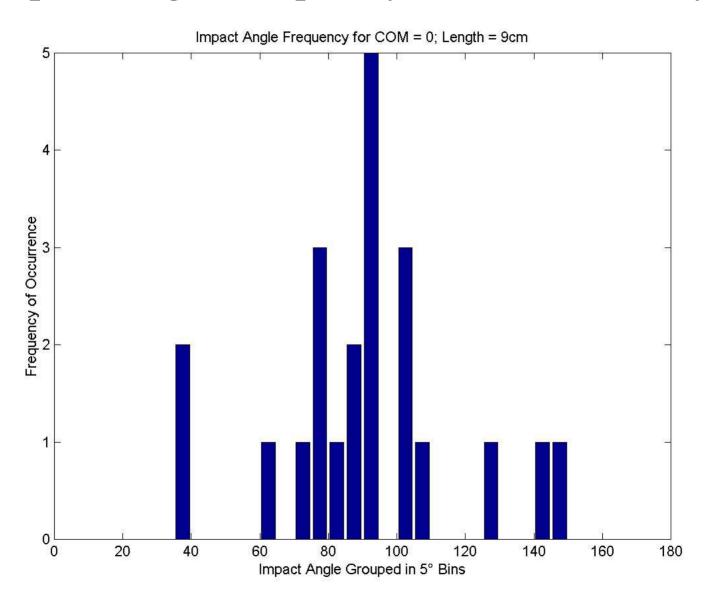


Impact Point (By Angle)

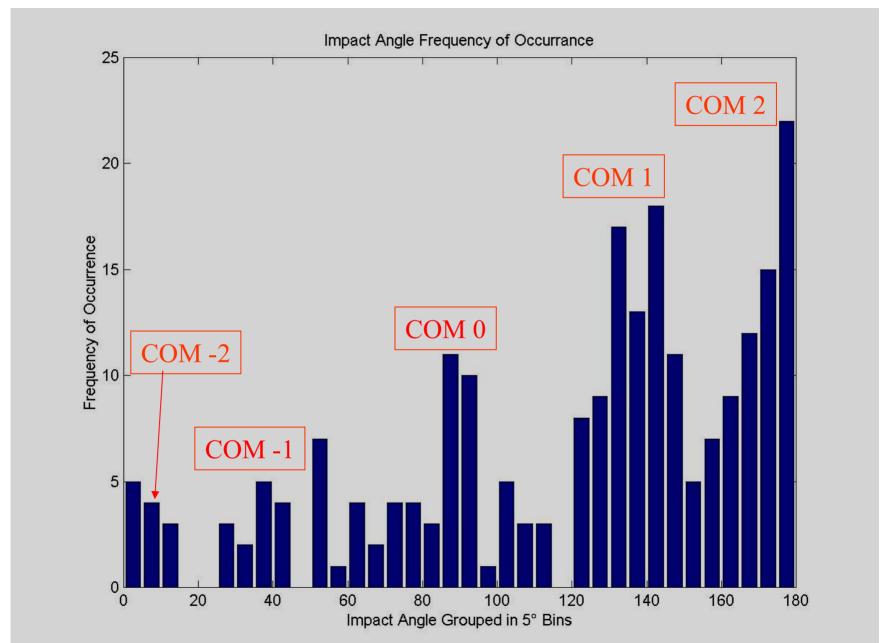




Impact Angle Frequency of Occurrence by L

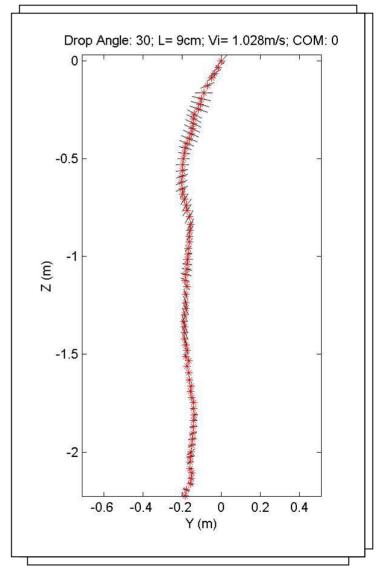


Impact Angle Frequency of Occurrence



Trajectory Patterns

- 1. Straight
- 2. Slant
- 3. Spiral
- 4. Flip
- 5. Flat
- 6. See Saw
- 7. Combination



Multiple Linear Regression

• General Multiple Linear Regression Equation:

$$\mathbf{f}_{1} = \beta_{0} + \beta_{1} \mathbf{x}_{11} + \beta_{2} \mathbf{x}_{21} + \beta_{3} \mathbf{x}_{31} + \beta_{4} \mathbf{x}_{41} + \varepsilon_{1}$$

- Used least squares solution to determine correlation coefficients.
- Input: cos(drop angle); L/D; V_{ind}; COM_{nd}
- Output: $(x_m, y_m, z_m, Psi, u, v, w)$

Multiple Regression Results

	Xm	Уm	Psi	u	V	W
β0	0746	0546	102.5691	.0040	0135	9481
β ₁	.1190	0828	-13.3508	0075	0106	1080
β ₂	0469	0798	5009	0011	.0005	.0295
β ₃	.0372	.0622	1.0437	.0025	.0011	0221
β4	.2369	.4330	472.2135	0090	.0537	-1.2467

• Most important parameter for impact prediction is Psi (impact angle).

Check of regression equation:

Determine Psi for case where:

L=15cm, $V_i = 3$ m/s, COM = 2, Drop Angle = 15°

Yields: $Psi = 181.2^{\circ}$

For COM = 1: Psi = 136.1°

For COM = 0: Psi = 90.4°

Conclusion

- COM position is the most influential parameter for predicting a mine's impact position and angle.
- Final velocities were lowest for COM 0 cases due to the increased effect of hydrodynamic drag.
- Trajectories became more complex as L/D decreased (9 cm mine rotated about z-axis).
- Observed trajectory patterns were more complex than those assumed by IMPACT 25. Accurate representation of a mine's water phase motion requires both momentum and moment of momentum equations.